S1 Appendix

Determination of the time derivative of the point of the blade where the water force vector is applied $(\dot{\vec{r}}_{PoA/w_{sg}})$. The expression of $\vec{r}_{PoA_{sg}}$ in an earth bound frame of reference is:

$$\vec{r}_{PoA/w_{sg}}(t) = \vec{r}_{d/w} + |\vec{r}_{T1/d}| \cdot \begin{pmatrix} \cos(\Phi_{d/w}) \\ \sin(\Phi_{d/w}) \end{pmatrix} \\ + \Delta^y_{oar_{sg_T}} \cdot \begin{pmatrix} -\sin(\Phi_{d/w}) \\ \cos(\Phi_{d/w}) \end{pmatrix} \\ + |\vec{r}_{PoA/T_{sg}}| \cdot \begin{pmatrix} \cos(\Phi_{d/w} + \Phi_{b/d_{sg}}) \\ \sin(\Phi_{d/w} + \Phi_{b/d_{sg}}) \end{pmatrix}$$
(A)

where $\vec{r}_{d/w}$ is the position vector of the oar pin in an earth-bound frame of reference. While in real rowing this information may be provided by a GPS, in our experiment the origin of the frames of references is at the oar pin and the $\vec{r}_{d/w}$ is thus zero. $\vec{r}_{T1/d}$ is the position vector of the beginning of the blade in the unloaded position. Calculation of $\vec{r}_{T/d}$ is based on the angle of the oar pin relative to the earth-bound frame of reference $(\Phi_{d/w})$ and the distance of the beginning of the blade from the oar. $\Delta^y_{oar_{sg_T}}$ is the position of the beginning of the blade in the loaded situation relative to the position of the beginning of the blade in the loaded situation relative to the position of the beginning of the blade in the loaded situation of $\vec{r}_{PoA/T_{sg}}$ is based on $|r_{PoA/T_{sg}}|$ and the angle of the blade relative to an earth-bound frame of reference $(\Phi_{b/w_{sg}} = \Phi_{d/w} + \Phi_{b/d_{sg}})$, both determined using the presented method. Therefore, $\vec{r}_{PoA/w_{sg}}$ is:

$$\begin{aligned} \dot{\vec{r}}_{PoA/w_{sg}} = \dot{\vec{r}}_{d/w} + |\vec{r}_{T/d}| \cdot \dot{\Phi}_{d/w} \cdot \begin{pmatrix} -\sin(\Phi_{d/w}) \\ \cos(\Phi_{d/w}) \end{pmatrix} \\ + \Delta oar_{sg_{T}}^{y} \cdot \begin{pmatrix} -\sin(\Phi_{d/w}) \\ \cos(\Phi_{d/w}) \end{pmatrix} + \Delta oar_{sg_{T}}^{y} \cdot \dot{\Phi}_{d/w} \cdot \begin{pmatrix} -\cos(\Phi_{d/w}) \\ -\sin(\Phi_{d/w}) \end{pmatrix} \\ + |\vec{r}_{PoA/T_{sg}}| \cdot \begin{pmatrix} \cos(\Phi_{d/w} + \Phi_{b/d_{sg}}) \\ \sin(\Phi_{d/w} + \Phi_{b/d_{sg}}) \end{pmatrix} \\ + |r_{PoA/T_{sg}}| \cdot (\dot{\Phi}_{d/w} + \dot{\Phi}_{b/d_{sg}}) \cdot \begin{pmatrix} -\sin(\Phi_{d/w} + \Phi_{b/d_{sg}}) \\ \cos(\Phi_{d/w} + \Phi_{b/d_{sg}}) \end{pmatrix} \end{aligned}$$
(B)